AMENDMENTS TO THE SPECIFICATION

Please replace the paragraph at page 3, lines 16 to 31 of the specification with the following amended paragraph.

A highly impact-resistant steel pipe according to ~~the claim 1~~ one embodiment of the present invention that is established for solving the aforementioned problems is characterized in that: the tensile strength (hereunder referred to as TS) of the steel pipe is 1,700 MPa or more; and the yield ratio (hereunder referred to as YR) thereof, the yield ratio being the ratio of the 0.1%-proof stress (hereunder referred to as YS) to the tensile strength TS (YS/TS), is 72% or less. Likewise, TS is 1,800 MPa or more and YR is 70% or less in ~~the claim 2~~ a second embodiment of the invention, TS is 1,900 MPa or more and YR is 68% or less in ~~the claim 3~~ a third embodiment thereof, and TS is 2,000 MPa or more and YR is 66% or less in ~~the claim 4~~ a fourth embodiment thereof. Here, it is preferable that the dislocation density of a steel pipe after a tensile test according to JIS is in the range from 10^{10} to 10^{14} /mm^{-2}.

Please replace the paragraph at page 4, lines 8 to 13 of the specification with the following amended paragraph.

The gist of ~~the claim 5~~ another embodiment of the present invention is a highly impact-resistant electric-resistance-welded steel pipe characterized by having a high strength of 1,700 MPa or more in tensile strength and being produced by controlling the Si amount in the steel of the steel pipe in the range from Mn/8 – 0.07 to Mn/8 + 0.07.

Please replace the paragraph at page 7, line 28 to page 8, line 4 of the specification with the following amended paragraph.

The present invention is hereunder explained in detail. A highly impact-resistant steel pipe according to the present invention ~~is, as described in claim 11, produced~~ is produced by subjecting a steel pipe containing, in mass 0.19 to 0.35% C, 0.1 to 0.3% Si, 0.5 to 1.6% Mn, not more than 0.025% P, not more than 0.02% S, 0.010 to 0.050% Al, 2 to 35 ppm B, and 0.005 to 0.05% Ti as indispensable components, and arbitrary components selected from among the group of 0.005 to 0.050% Nb, 0.005 to 0.070% V, 0.005 to 0.5% Cu, 0.005 to 0.5% Cr, 0.1 to 0.5% Mo, 0.1 to 0.5% Ni, not more than 0.01% Ca, and not more than 0.1% rare earth metals (REMs) to induction heating and then water quenching. The reason for regulating the amount of each component is explained below.

Please replace the paragraph at page 7, lines 5 to 21 of the specification with the following amended paragraph.

C is a component indispensable for strengthening martensite itself and thus enhancing hardness and must be added by at least 0.19% for securing a TS value of 1,700 MPa or more. However, an excessive C amount makes a martensite structure brittle and baking cracks that cause fracture during quenching occur. Therefore, a C amount is set at not more than 0.35%. Further, it is preferable to set a C amount: at about 0.21% for obtaining a steel pipe having a TS of 1,700 MPa or more and a YR of 72% or less ~~according to the claim 1 of the present invention~~; at about 0.24% for a steel pipe having a TS of 1,800 MPa or more and a YR of 70% or less ~~according to the claim 2~~; at about 0.28% for a steel pipe having a TS of 1,900 MPa or more and a YR of 68% or less ~~according to the claim 3~~; and at about 0.30% for a steel pipe having a TS of 2,000 MPa or more and a YR of 66% or less ~~according to the claim 4~~.

Please replace the paragraph at page 11, line 34 to page 12, line 20 of the specification with the following amended paragraph.

~~Further, as shown in the claim 9, it~~ Further, it is preferable that 95% or more of the microstructure of a steel pipe is transformed into martensite by induction hardening and the prior austenite grain size number of the steel pipe is #6 or more particularly for securing a low temperature impact bending property. Fig. 5 is a graph showing the result obtained by subjecting highly impact-resistant electric-resistance-welded steel pipes (1,700 MPa in tensile strength) having various prior austenite grain size numbers to impact bending tests and observing the occurrence of cracks. From Fig. 5, it is understood that steel pipes having an excellent low temperature impact bending property are obtained by securing minute crystals having prior austenite grain size numbers of #6 or more. Here, crystals can be fractionized by the effect of, for example, lowering a hardening temperature, fractionizing the grains of a pre-hardening structure, adding elements such as Nb, V, Ti, etc., or the like. A prior austenite grain size number may be measured by exposing the boundaries of prior austenite grains in a base material with a generally used austenite grain boundary exposing liquid and thereafter employing a cutting method or an image analysis method.